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The University of Calgary
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ENCH 501: Transport Processes Quiz #6

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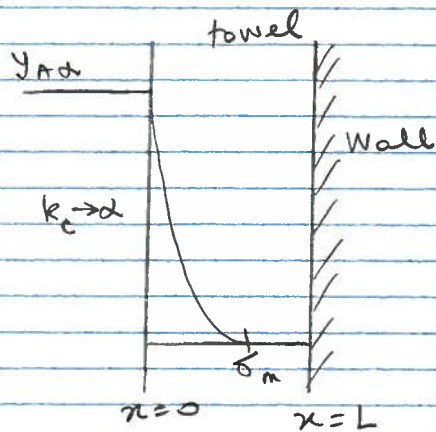
Time Allowed: 40 mins.

Name: _____

Hydrogen sulphide, H_2S , is a very toxic compound to mammals, even in low concentrations in air. It must, therefore, be removed as quickly as possible, particularly from an enclosed space. When a cannister of the gas accidentally discharged its content into a small, enclosed analytical laboratory, the manager instructed that a thick towel be soaked in an alkali (or amine) solution and the excess liquid squeezed out. The towel then becomes a porous medium with a thin layer of alkali covering the fibers. The towel is then pinned to a wall. As H_2S from the air diffuses into the towel, the gas also reacts with the alkali to form a complex held on the towel fibers.

You are given that the thickness of the towel is L and the towel initially contained no H_2S . Because the towel is mounted on a wall, you may assume that the towel side at the wall is impervious. The gas in the towel occupies a void fraction ϵ . The reaction in the towel is first order, i.e. the rate of removal of H_2S is proportional to the local concentration of H_2S in the gas. The rate is also proportional to the fraction of the towel occupied by the fibers. Assume the rate constant is k_1 . At the ambient air side of the towel, the mole fraction of H_2S in the air, $y_{A\infty}$, is substantial (about 20%) and the air is rapidly moved around by a fan such that it may be assumed that the mass transfer coefficient (k_c) at the open towel surface is very large. The temperature and pressure in the room are constant at T and P . Assume that the air within the towel is stagnant.

- a) Use the **integral method** to derive an expression for the concentration profile for H_2S $y_A(x,t)$ in the towel, up to the instant the compound has just penetrated to the face of the towel at the wall. Show all your steps.
- b) How would you estimate the total amount of H_2S removed by the towel at this instant?



□ Because of the air movement outside, $k_c \rightarrow \infty$, and therefore the concentration of H_2S (substance A) at $x=0$ is given by

$$C_A = C_{A\infty} = C y_{A\infty}; C = \frac{P}{RT}$$

□ This is a semi-infinite domain problem since $\delta_m \leq L$

□ The flux of A is given by (within the towel)

$$N_{Ax} = -C D_{AB} \epsilon \frac{dy_A}{dx} + y_A (N_A + N_B)$$

where B is the air in the pore space of the towel.

The air is stagnant, hence $N_B = 0$

$$\therefore N_{Ax} = -C D_{AB} \epsilon \frac{dy_A}{1-y_A dx} \quad (1)$$

□ Let the control volume be the towel, $0 \leq x \leq L$

$$\text{Input} + \text{Generation} = \text{Output} + \text{Accum}$$

$$\text{Input per unit area} = N_{Ax} \Big|_{x=0} = -C D_{AB} \epsilon \frac{dy_A}{1-y_A dx} \Big|_{x=0}$$

$$\text{Generation per unit towel surface area} = \int_0^{\delta_m} -k_1 (1-\epsilon) C y_A dx$$

$$\text{Accum} = \frac{d}{dt} \left[\int_0^{\delta_m} \epsilon C y_A dx \right]$$

The upper limits of both integrals are δ_m because $y_A = 0$ for $\delta_m < x \leq L$

The integral material balance equation is

$$\left. - \frac{c_{AB} E}{1-y_A} \frac{dy_A}{dx} \right|_{x=0} - \int_0^{\delta_m} k_1 (1-E) c y_A dx = \frac{d}{dt} \left[\int_0^{\delta_m} E c y_A dx \right]$$

or

$$\left. - \frac{D_{AB}}{1-y_{Ax}} \frac{dy_A}{dx} \right|_{x=0} - k_1 \left(\frac{1-E}{E} \right) \int_0^{\delta_m} y_A dx = \frac{d}{dt} \left[\int_0^{\delta_m} y_A dx \right] \quad (2)$$

□ Identify the b.c.

$$x=0 \quad y_A = y_{Ax}$$

$$x=\delta_m \quad y_A = 0$$

$$x=\delta_m \quad \frac{dy_A}{dx} = 0$$

Assume profile $y_A = a + bx + cx^2$

Apply b.c.

$$\frac{y_A}{y_{Ax}} = \left(1 - 2 \frac{x}{\delta_m} + \frac{x^2}{\delta_m^2} \right) = \left(1 - \frac{x}{\delta_m} \right)^2 \quad (3)$$

$$\left. \frac{dy_A}{dx} \right|_{x=0} = - \frac{2 y_{Ax}}{\delta_m} + \frac{2x y_{Ax}}{\delta_m^2}$$

$$\begin{aligned} y_{Ax} \int_0^{\delta_m} \left(1 - 2 \frac{x}{\delta_m} + \frac{x^2}{\delta_m^2} \right) dx &= y_{Ax} \left(x - \frac{x^2}{\delta_m} + \frac{1}{3} \frac{x^3}{\delta_m^2} \right) \Big|_0^{\delta_m} \\ &= y_{Ax} \frac{\delta_m}{3} \end{aligned}$$

Substitute these into equation (2)

$$- \frac{D_{AB}}{1-y_{A\alpha}} \left(- \frac{2 y_{A\alpha}}{\delta_m} \right) - k_1 \left(\frac{1-\epsilon}{\epsilon} \right) \frac{y_{A\alpha} \delta_m}{3} = \frac{d}{dt} \left[y_{A\alpha} \frac{\delta_m}{3} \right]$$

or

(3)

$$\frac{6 D_{AB}}{1-y_{A\alpha}} \frac{1}{\delta_m} - k_1 \left(\frac{1-\epsilon}{\epsilon} \right) \delta_m = \frac{d}{dt} \delta_m$$

or

$$\alpha - \beta \delta_m^2 = \frac{d\delta_m^2}{dt}; \quad \alpha = \frac{12 D_{AB}}{1-y_{A\alpha}}$$

$$\beta = 2k_1 \left(\frac{1-\epsilon}{\epsilon} \right)$$

Subject to the condition

$$t=0, \quad \delta_m=0$$

$$\text{Let } Y = \alpha - \beta \delta_m^2 \quad \therefore dY = -\beta d\delta_m^2$$

\therefore eq. becomes

$$\frac{dY}{Y} = -\beta dt = d \ln Y$$

Integrate

$$\int_{Y=\alpha}^Y d \ln Y = - \int_0^t \beta dt$$

$$\ln \frac{Y}{\alpha} = -\beta t \quad \text{or} \quad Y = \alpha e^{-\beta t}$$

$$\text{i.e.} \quad \alpha - \beta \delta_m^2 = \alpha e^{-\beta t}$$

$$\text{or} \quad \delta_m = \left[\frac{\alpha}{\beta} (1 - e^{-\beta t}) \right]^{\frac{1}{2}} \quad (4)$$

Substitute this into eq. (3) for profile. \rightarrow

- (b) At the instant $S_m = L$, equation (4) can be used to estimate the time, τ .

The total uptake of H_2S can be estimated from

$$Q = \int_0^{\tau} N_A|_{x=0} dt$$

$$= \frac{-c D_{AB} E}{1 - y_{Ad}} \int_0^{\tau} \left. \frac{dy_A}{dx} \right|_{x=0} dt$$

or from both amount reacted and still diffusing.

That is:

$$Q = \int_0^L \left[\int_0^{\tau} k_1 (1 - \epsilon) c y_A dt \right] dx +$$

$$\int_0^L c y_A \epsilon dx$$

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