

The University of Calgary  
Department of Chemical & Petroleum Engineering

**ENCH 501 : Mathematical Methods in Chemical Engineering**  
**Quiz #6**

**Time Allowed: 50 min.**

**November 20, 2001 AJ**

---

A barge containing 0.2 million barrels of crude oil was involved in an accident in the middle of a large calm lake and the vessel broke into two parts, spilling its entire cargo. The oil formed a circular patch of a thickness of 1.6 cm initially on the lake. Then it started to spread. Given the assumptions and data below,

- i) Plot the radius versus time pattern for the oil layer and explain your method and reasoning;
- ii) Estimate how long the oil slick will take for its thickness to decrease to 1 mm.

**Assumptions and Data:**

- 1) There are three regimes of spreading and the transitions between the regimes occur at oil layer thicknesses of 0.65 and 0.2 cm.
- 2) One barrel of oil is equivalent to 159 litres.
- 3) Densities of water and oil are 998 and 952 kg/m<sup>3</sup> respectively.
- 4) The interfacial tension between oil and water is 0.025 N/m.
- 5) Viscosity of water is 1.6 mPa.s.
- 6) The oil is more viscous than water; it does not vaporize, expand or contract over the period of interest. The oil neither absorbs substances from water nor releases compounds into the water. There is also no biological activity.
- 7) There are no currents in the lake and the air is still.

Volume spilled = 0.2 m barrels or  $V = 31,800 \text{ m}^3$

Given the patch is a disc,  $\pi R^2 h = V$

$$h = 1.6 \text{ cm} \text{ or } 0.016 \text{ m}$$

$$\text{At } t=0, R = 795.39 \text{ m}$$

$$\text{When } h = 1 \text{ mm or } 0.001 \text{ m, } R = 3181.55 \text{ m.}$$

$$h = 6.5 \text{ mm or } 0.0065 \text{ m } R = 1247.9 \text{ m}$$

$$\text{and } h = 2 \text{ mm } R = 2249.7 \text{ m}$$

$$\Delta = \frac{998 - 952}{998} \approx 0.046$$

$$\mu = 1.6 \text{ mPa.s} \text{ or } 1.6(10^{-3}) \text{ m}^2/\text{s.}$$

(c) first stage of spreading - Dominant forces - gravity + inertia

$$\text{By order of magnitude, } R \sim \sqrt[4]{(g \Delta t)^{\frac{1}{4}} + \frac{1}{2}} \quad (\text{from Notes})$$

for second stage, Dominant forces - gravity + viscous

$$\text{and } R \sim 2^{-\frac{1}{2}} (g \Delta)^{\frac{1}{16}} t^{\frac{1}{3}} \quad (2^{\frac{1}{4}} \sim 1.19)$$

and for 3rd stage, Dominant forces - surface tension + viscous

$$R \sim \sqrt[2]{(\rho \mu)^{\frac{1}{4}}} t^{\frac{3}{4}} \quad (3)$$

Time  $t$  has entered into all three relationships (as shown with Notes) from velocity, acceleration or rate of change. It is not absolute time. Only for the first one is time relative to the start of spreading!

If a log-log plot is used, eq. (1) becomes

$$\ln\left(\frac{R}{\beta}\right) \sim \frac{1}{2} \ln t \quad ; \quad \beta = (g \Delta t)^{\frac{1}{4}}$$

and both sides are dimensionally consistent.

$$\text{When } R = 795.39 \text{ m}, \quad t = 5281 \text{ s}$$

Use log-log plot + locate point.

Draw line slope  $\frac{1}{2}$  to  $R = 1248 \text{ m}$ .

In  $1248 < R < 2250 \text{ m}$ , draw slope  $\frac{1}{4}$

for  $R > 2250 \text{ m}$ , draw slope  $\frac{3}{4}$ .  $\rightarrow$

(b) final time  $\sim 246,000 \text{ s}$  for  $h = 1 \text{ mm}$

$$\text{Time difference} = (246,000 - 5281) = 66,877 \text{ hrs} \rightarrow \\ < 2.8 \text{ days.}$$

Alternate.  for the different regimes.

$$R_1 - R_0 = (g \Delta t)^{\frac{1}{4}} (t^{\frac{1}{2}}) \quad t \sim 1708 \Rightarrow$$

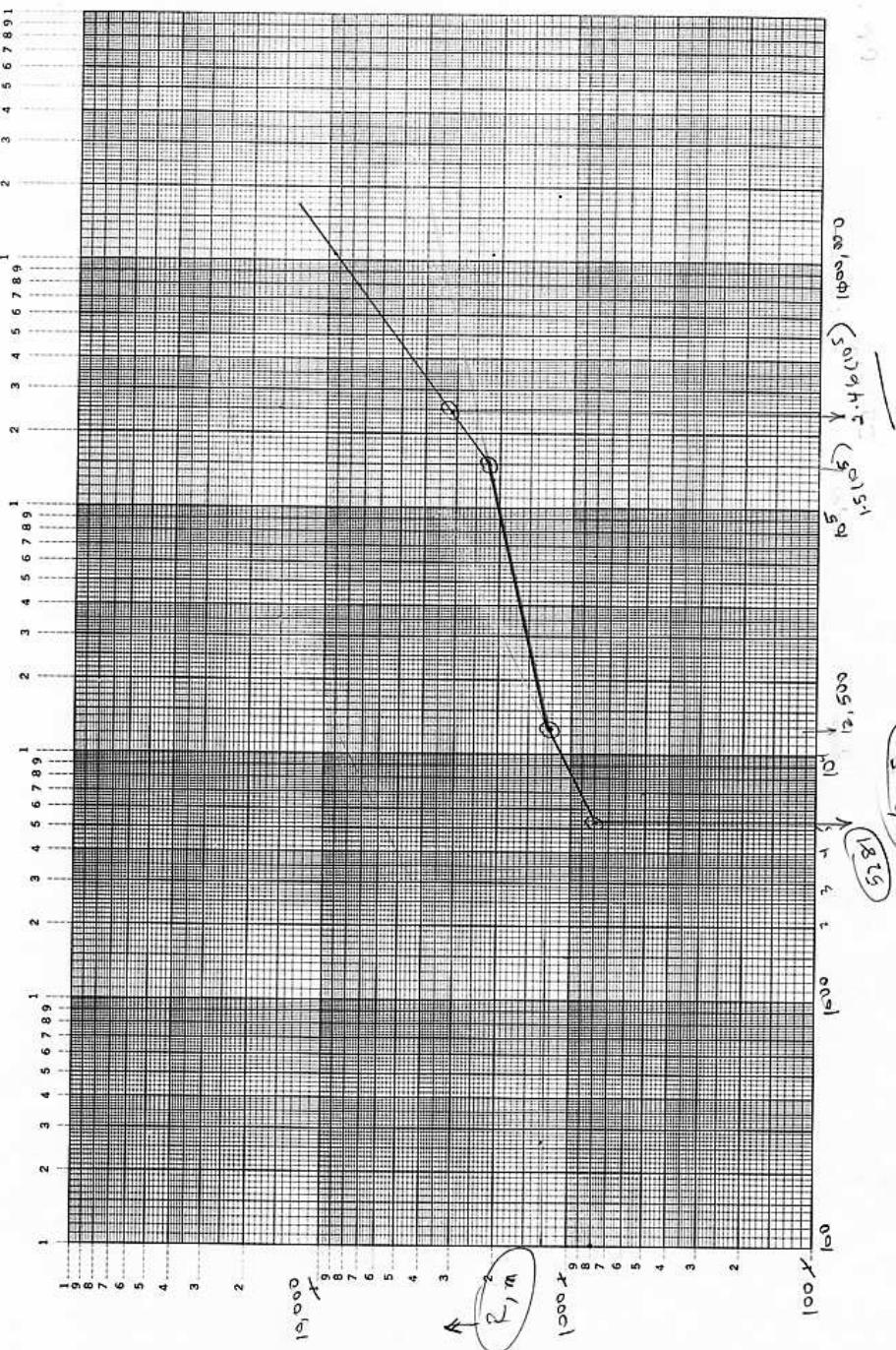
$$R_2 - R_1 = \nu^{-\frac{1}{12}} (g \Delta t)^{\frac{1}{4}} t^{\frac{1}{3}} [t_2^{\frac{1}{4}} - t_1^{\frac{1}{4}}] \quad t_2 \sim 1.12 (10^5) \text{ s}$$

$$R_3 - R_2 = \nu^{-\frac{1}{12}} (\rho \mu)^{\frac{1}{4}} [t_3^{\frac{3}{4}} - t_2^{\frac{3}{4}}] \quad t_3 \sim 2.968 (10^5) \text{ s}$$

$$\therefore \text{time} \sim 82.45 \text{ hrs.}$$

K-E LOGARITHMIC 3 X 5 CYCLES  
KEUFFEL & ESSER CO. MADE IN U.S.A.

46 7520



Oil Spreading on Calm Water.

4 basic forces - cause retardation

$$P_0 = \rho_w (1 - \Delta) ; \Delta \ll 1$$

oil is hydrostatic in vertical direction

$$P_0 h = \rho_w g$$

$$y = (1 - \Delta) h , \text{ i.e. } Dh \text{ is}$$

above mean water surface.

$$\leftarrow \frac{1}{2} \rho g Dh$$

$$\text{more accurately, force on semi-circular contact area} \\ = \frac{1}{2} \rho w g h (1 - \Delta) \Delta \times \text{area}$$

$$\text{pressure } F \approx (\rho g Dh)(1h) . (2/1)$$

$$\text{gravity mass } \propto \text{area} \sim \rho h l^2 \left( \frac{l}{r^2} \right)$$

$$\text{viscous } \mu \frac{du}{dx} \cdot 2\pi r dr \sim \mu \left( \frac{l}{r} \right)^2 \cdot l^2 \\ \approx \sim \sqrt{\nu t}$$

interfacial

$$\sigma t$$

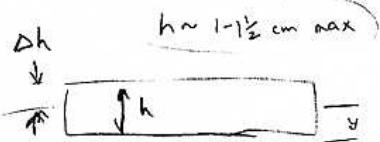
stokes first problem

$t \rightarrow 0$

gravity > surface tension

$$h > \left[ \frac{\sigma}{\rho g \Delta} \right]^{\frac{1}{2}} \sim 1 \text{ cm} ; V \propto h l^2$$

From Notes



pressure (gravity) - causes spreading  
inertia - retardation

viscous - retardation

interfacial tension - const.

neglect - evaporation  
lighter vapour  
dissolution  
water  
biological degradation

①

long time

$h \rightarrow 0$

viscous / surface tension

$$l = 1.33 \tau^{\frac{1}{2}} \left( \frac{\rho}{\mu} \right)^{\frac{1}{4}} t^{\frac{3}{4}}$$

of volume released

② short time

pressure / inertia.

gravity / inertia

$$l \sim [5 \Delta \tau]^{\frac{1}{4}} t^{\frac{1}{2}} \\ \frac{dl}{dt} \sim t^{-\frac{1}{2}}$$

gravity / viscous  
viscous  $l \sim \tau^{-\frac{1}{2}} (5 \Delta)^{\frac{1}{4}} t^{\frac{1}{3}} t^{\frac{1}{4}}$   
 $\frac{dl}{dt} \sim t^{-\frac{3}{4}}$

surface tension / viscous  
 $l \sim \sigma^{\frac{1}{2}} \left( \frac{\rho}{\mu} \right)^{\frac{1}{4}} t^{\frac{3}{4}}$   
 $\frac{dl}{dt} \sim t^{-\frac{1}{4}}$