

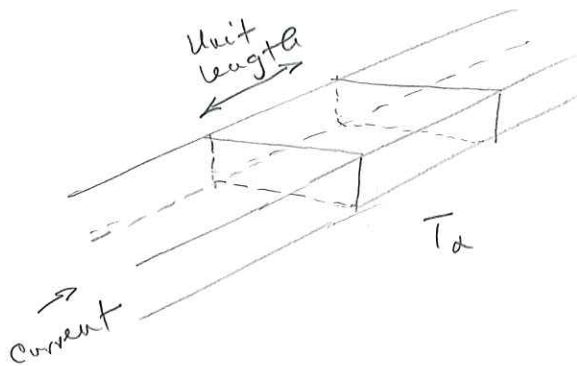
November 6, 2018 Time Allowed: 45 minutes

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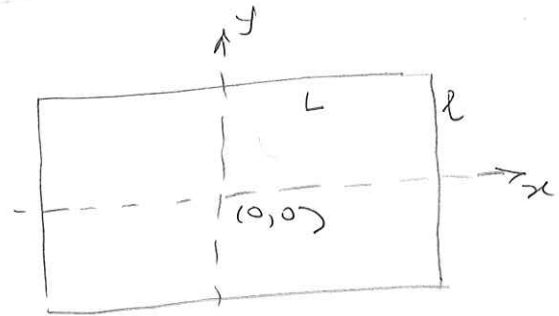
The cross-section of a long metal bar is rectangular, and the bar is initially at the same temperature as the ambient air at T_a . The flow of an electric current is suddenly started through the bar so that heat is generated uniformly and at a constant rate per unit volume $\dot{g}$ within the bar. If the bar cross-section is $2L$ (along the x-direction) by $2l$ (along the y-direction), obtain a relationship for $T(x,y,t)$ at the cross-section by the **integral** method. Assume that the heat transfer coefficient at the surfaces of the bar h is infinite and the properties of the metal – ρ , C_p and k are constants. Show important steps.

Hints: Consider a unit length of the bar. Until steady state, some of the heat generated will be stored in the bar. At any instant, the energy content of a unit length of the bar may be obtained by first considering the energy content of a dx by dy by 1 volume of the bar. Then all the energy for similar elements at the cross-section are added. A double integral is in the accumulation term.

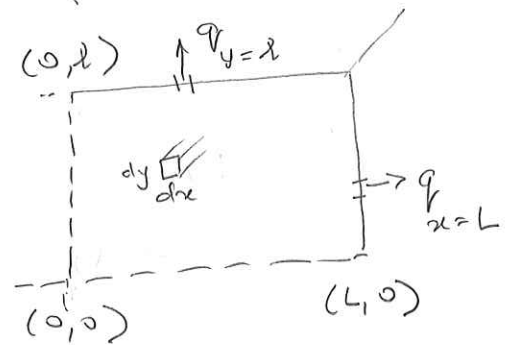
Do not spend much time re-deriving what is in your notes. Use any relevant previous results but give enough steps that a reader can follow your analysis.



The cross section is like



The temperature field $T(x, y, t)$ will be determined for a quadrant as the lines $x=0$ and $y=0$ represents planes of symmetry.



The energy balance equation for the control volume (the quadrant with unit length along the bar) by the integral method is

$$\text{Input} + \text{Generation} = \text{Output} + \text{Accumulation}$$

$$\text{Generation rate} = \dot{q}^+ L l$$

$$\text{Output rate} = \int_0^l \dot{q}_{x=L} dy + \int_0^L \dot{q}_{y=l} dx$$

$$\text{Accumulation} = \frac{d}{dt} \left[\int_0^l \int_0^L \rho (dx dy) C_p (T(x, y, t) - T_a) \right]$$

2

integral
The energy equation is

$$g^+ L^2 = \int_0^L -k \left. \frac{\partial T}{\partial x} \right|_{x=L} dy + \int_0^L -k \left. \frac{\partial T}{\partial y} \right|_{y=1} dx + \frac{\partial}{\partial t} \left[\int_0^L \int_0^L \rho c_p (T - T_\infty) dx dy \right] \quad (1)$$

Let $\theta(x, y, t) = T(x, y, t) - T_\infty$

Also, let the solution be separable, i.e.

$$\theta(x, y, t) = X(x) Y(y) T(t)$$

where $X(x)$ and $Y(y)$ have to be even functions to satisfy the symmetry conditions.

At long times, the heat generated equals the heat output and accumulation equals zero.

Hence $X(x) Y(y)$ is the steady state solution

as $T(t)$ equals a constant, say 1.

At short times, $T(x, y, t) = T_\infty \Rightarrow T(0) = 0$

Assume that

$$\theta(x, y, t) = a_0 (L^2 - x^2)(L^2 - y^2) T(t) \quad (2)$$

This satisfies the conditions -

$$x=0 \quad \frac{\partial \bar{T}}{\partial x} = 0 \quad (\text{symmetry})$$

$$y=0 \quad \frac{\partial \bar{T}}{\partial y} = 0 \quad \checkmark$$

$$x=L \quad T = \bar{T}_2 \quad (h \rightarrow \infty)$$

$$y=l \quad T = \bar{T}_2 \quad \checkmark$$

The steady state solution (see Notes) is obtained by substituting the profile

$$\theta(x, y, t) = a_0 (L^2 - x^2) (l^2 - y^2)$$

into the integral energy equation without the accumulation term. This gives

$$a_0 = \frac{3}{4} \frac{g^+ / k}{L^2 + l^2} \quad (3)$$

The gradients in the output terms are obtained as

$$\left. \frac{\partial \bar{T}}{\partial x} \right|_{x=L} = -2L a_0 (l^2 - y^2) \Gamma(t) \quad (4a, b)$$

$$\left. \frac{\partial \bar{T}}{\partial y} \right|_{y=l} = -2l a_0 (L^2 - x^2) \Gamma(t)$$

Substitute equations 2 and 4 into equation 1, and simplify

$$\begin{aligned}
 g^+ L l &= 2k L a_0 \Gamma(t) \int_0^l (l^2 - y^2) dy + \\
 & 2k l a_0 \Gamma(t) \int_0^L (L^2 - x^2) dx + \\
 & \frac{\partial}{\partial t} \left[\int_0^l \int_0^L \rho C_p a_0 (L^2 - x^2)(l^2 - y^2) \Gamma(t) dx dy \right] \quad (5)
 \end{aligned}$$

$$\begin{aligned}
 g^+ L l &= \frac{4}{3} k a_0 (L l^3 + l L^3) \Gamma(t) + \\
 & \rho C_p a_0 \frac{d}{dt} \left[\Gamma(t) \cdot \frac{4}{9} L^3 l^3 \right]
 \end{aligned}$$

This equation is of the form

$$\frac{d}{dt} \Gamma(t) + a \Gamma(t) = b \quad (6)$$

$$\text{where } a = \frac{4/3 k a_0 (L l^3 + l L^3)}{4/9 L^3 l^3 \rho C_p a_0} \quad \left| \begin{array}{l} \text{both} \\ \text{constants} \end{array} \right.$$

$$\text{and } b = \frac{g^+ L l}{\frac{4}{9} L^3 l^3 \rho C_p a_0}$$

This equation is subject to the condition $t=0 \quad \bar{T}=0$

Re-arrange equation

$$d \ln(b - a\bar{T}(t)) = -a dt$$

$$\text{or } \ln(b - a\bar{T}) = -at + c$$

Apply condition

$$c = \ln b$$

$$\therefore \ln\left(\frac{b - a\bar{T}}{b}\right) = -at$$

$$\text{or } 1 - \frac{a}{b}\bar{T} = e^{-at}$$

$$\therefore \bar{T}(t) = \frac{b}{a}(1 - e^{-at}) \quad (7)$$

Substitute equations (3), and (7) into equation (2) to obtain the transient profile

$$\bar{\theta}(x, y, t) = \bar{T}(x, y, t) - \bar{T}_\infty = a_0(l^2 - x^2)(l^2 - y^2) \cdot \frac{b}{a}(1 - e^{-at})$$