

The University of Calgary
Department of Chemical & Petroleum Engineering

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ENCH 501: Transport Processes Quiz #4

October 18, 2002

Time Allowed: 50 mins.

Name: _____

Problem #1 (5 points)

Heat is generated at a constant and uniform rate, g' per unit volume, in a flat plate. The plate has a thickness $2L$ and it is contacted with a large reservoir of air on both sides at a temperature T_∞ . The heat transfer coefficient h is the same on both exposed surfaces.

If the plate was at an initial temperature T_0 before the heat generation started, use the Integral Method to derive a function for the temperature in the plate as a function of space and time, i.e. $T(x,t)$. Show all your steps and state your assumptions.

Problem #2 (5 points)

In cold climates, heavy-oil-gathering pipes, pipes in oil refineries or chemical plants exposed to ambient are often "heat traced". A method is to run an insulated electrical cable or ribbon filament along the length of the pipe and pass a current through the wire. The heat generated is transferred to the pipe and it keeps the material flowing within warm. You are instructed by your boss to heat trace a pipe using a thin ribbon coated with a thin plastic layer. The plastic starts to soften and degrade at a temperature of 130°C . So you decided to conduct a test first.

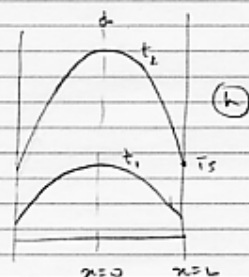
The ribbon available is molybdenum, 1mm thick, and it is wide enough that you can assume it is an infinite plate. The initial temperature of the ribbon is -8°C . You pass a current through so that heat is generated at 39.192 MW/m^3 .

- (a) If your test ribbon is uninsulated and exposed to air at -8°C on both sides, what is the value for the heat transfer coefficient (h) below which the ribbon surface temperature will attain or exceed 130°C ?
- (b) For the condition in part (a), what is the temperature at the midplane of the ribbon 5s after heat generation started?

Data: Properties of Molybdenum

$$k = 118 \text{ W/m K} ; C_p = 0.251 \text{ kJ/kg K} ; \rho = 10,220 \text{ kg/m}^3$$

Problem #1



Energy balance over the region

$$0 \leq x \leq L$$

$$\frac{d}{dt} \left[\int_0^L \rho C_p (\bar{T} - \bar{T}_a) dx \right] - \underbrace{g^+ L}_{\text{accum}} = \underbrace{-q^-}_{\text{gen}} \bigg|_{x=L} \quad \text{output}$$

Subject to

i.e. $t=0 \quad \bar{T} = T_a$

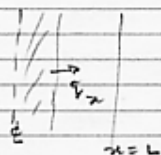
b.c. $x=0 \quad \frac{d\bar{T}}{dx} = 0$ symmetry

convective $x=L \quad -k \frac{d\bar{T}}{dx} \bigg|_L = h(\bar{T}_L - \bar{T}_a)$

Assume $\bar{T} - \bar{T}_a = X(x) \bar{T}(t)$ where $X(x)$ is the steady state solution and $\bar{T}(t) \rightarrow 1$ as $t \rightarrow \infty$

Also $\bar{T}(t) = 0$ at $t = 0$

Find first $X(x)$, the steady state solution



Energy balance on shaded element

$$g^+ dx = -k \frac{d^2 \bar{T}}{dx^2} dx$$

Integrate

$$-\frac{g^+}{k} \int_0^L x dx = \int_{\bar{T}}^{\bar{T}_s} d\bar{T}$$

$$\text{or } \frac{1}{2} \left(-\frac{g^+}{k} \right) (L^2 - x^2) = (\bar{T}_s - \bar{T})$$

But at $x=L \quad -k \frac{d\bar{T}}{dx} = g^+ L = h(\bar{T}_s - \bar{T}_a)$

$$\text{or } \bar{T}_s - \bar{T}_a = \frac{g^+ L}{h}$$

$$\therefore -\frac{1}{2} \left(\frac{q^+ L^2}{k} \right) \left(1 - \frac{x^2}{L^2} \right) = T_a + \frac{q^+ L}{h} - T$$

$$\begin{aligned} \text{or } (T - T_a) &= \frac{q^+ L}{h} - \frac{1}{2} \left(\frac{q^+ L^2}{k} \right) \left(1 - \frac{x^2}{L^2} \right) \\ &= \frac{1}{2} \frac{q^+ L^2}{k} \left[\frac{2k}{hL} + 1 - \frac{x^2}{L^2} \right] \end{aligned}$$

Hence the steady profile is

$$T(x, \infty) - T_a = \frac{1}{2} \frac{q^+ L^2}{k} \left\{ 1 - \frac{x^2}{L^2} + \frac{2}{Bi} \right\}$$

where $Bi \neq 0$, $Bi = hL/k$.

The transient temperature profile is

$$\frac{T - T_a}{\left(\frac{q^+ L^2}{k} \right)} = \frac{1}{2} \left[1 - \frac{x^2}{L^2} + \frac{2k}{hL} \right] \Gamma'(x)$$

Substitute into

$$\frac{d}{dt} \left[\int_0^L \rho c_p (T - T_a) dx \right] - q^+ L = k \left. \frac{dT}{dx} \right|_{x=L}$$

to yield

$$\frac{1}{1 - \Gamma} \frac{d\Gamma}{dt} = \left(\frac{Bi}{Bi + 3} \right) \frac{3x}{L^2}$$

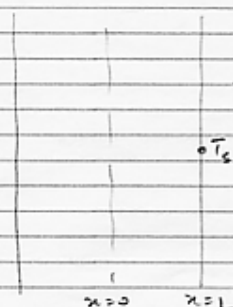
subject to $t = 0$ $\Gamma = 0$

$$\text{solve: } \Gamma = 1 - \exp \left(- \frac{3xt}{L^2} \frac{Bi}{Bi + 3} \right)$$

Hence final solution

$$\frac{T - T_a}{\left(\frac{q^+ L^2}{k} \right)} = \frac{1}{2} \left[1 - \frac{x^2}{L^2} + \frac{2}{Bi} \right] \left[1 - \exp \left(- \frac{3xt}{L^2} \frac{Bi}{Bi + 3} \right) \right]$$

Problem #2



(a) At steady state

$$q'' L = h (T_s - T_a)$$

$$T_s = 130^\circ\text{C}, T_a = -8^\circ\text{C}$$

$$h = \frac{39.192(10^6)(0.5)(10^{-3})}{138}$$

$$= 142 \text{ W/m}^2\text{K} \rightarrow$$

(b) Use the solution in problem #1

$$Bi = \frac{hL}{k} = \frac{142(0.5)(10^{-3})}{118} = 6.0165(10^{-4})$$

$$\alpha = \frac{k}{\rho c_p} = \frac{118}{10320(251)} = 4.6(10^{-5}) \text{ m}^2/\text{s}$$

$$\exp\left[-\frac{3\alpha t}{L^2} \cdot \frac{Bi}{Bi+3}\right] = \exp\left[-0.11069 \times 5\right] = 0.575$$

$$T|_{x=0} = -8 + \frac{39.192(10^6)(0.5)^2(10^{-6})}{138} \cdot \frac{1}{2} \left[1 + \frac{2}{6.0165(10^{-4})}\right]$$

$$= -8 + 138.04(1 - 0.575)$$

$$= 50.67^\circ\text{C} \rightarrow$$